

Mextram 504

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Willy Kloosterman**

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Mextram 504

**Philips
Research**

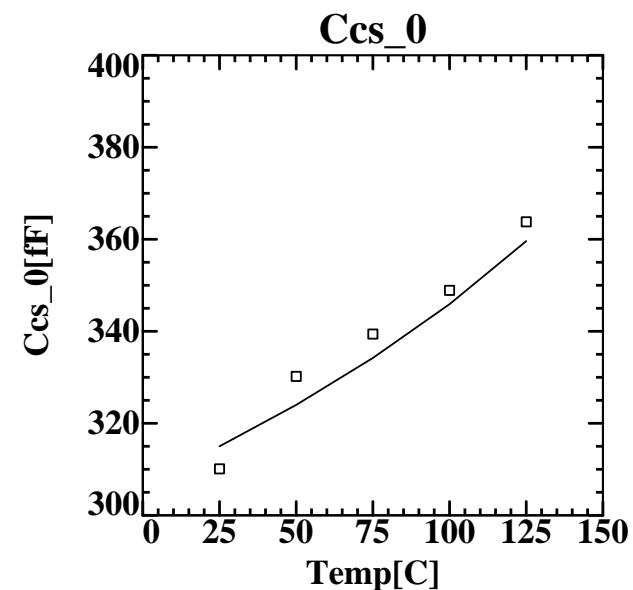
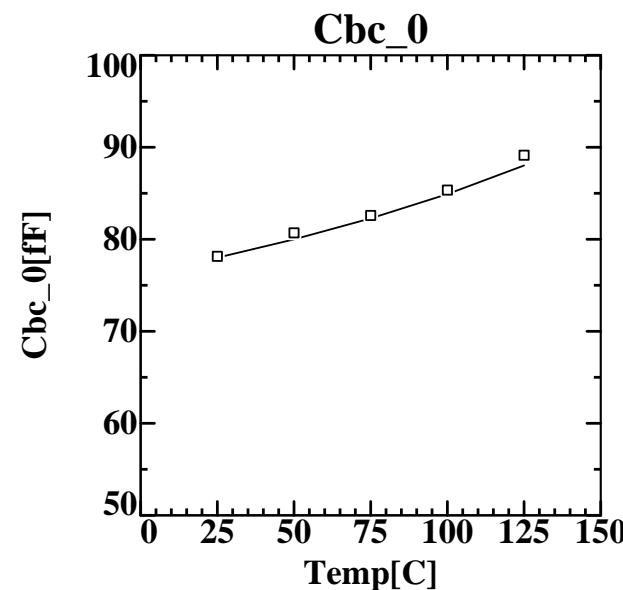
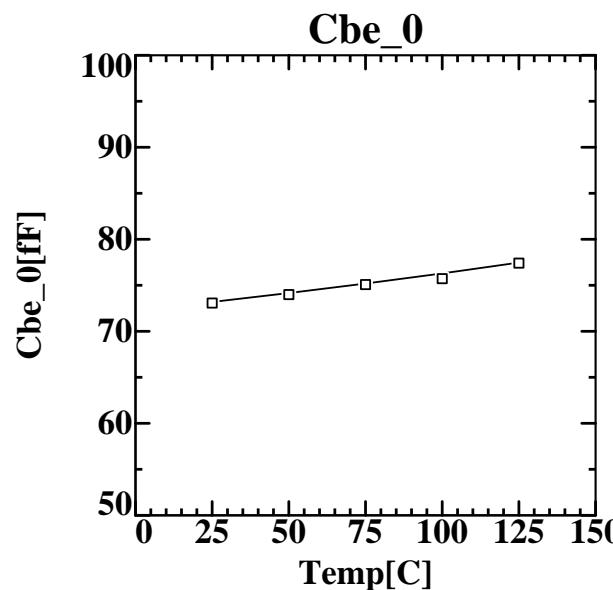
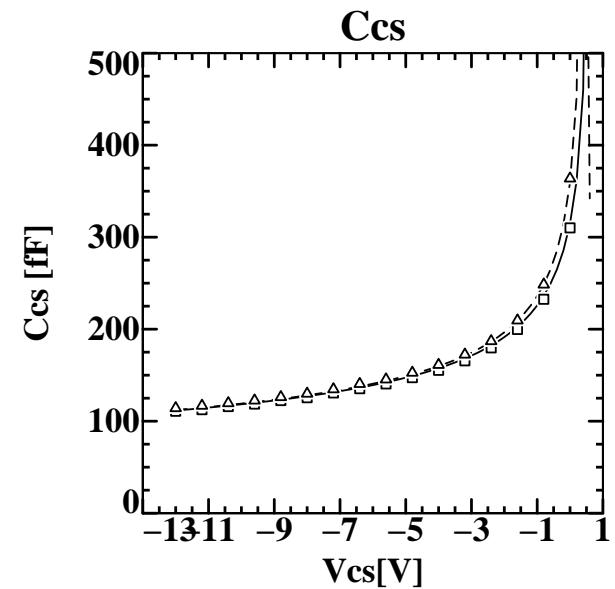
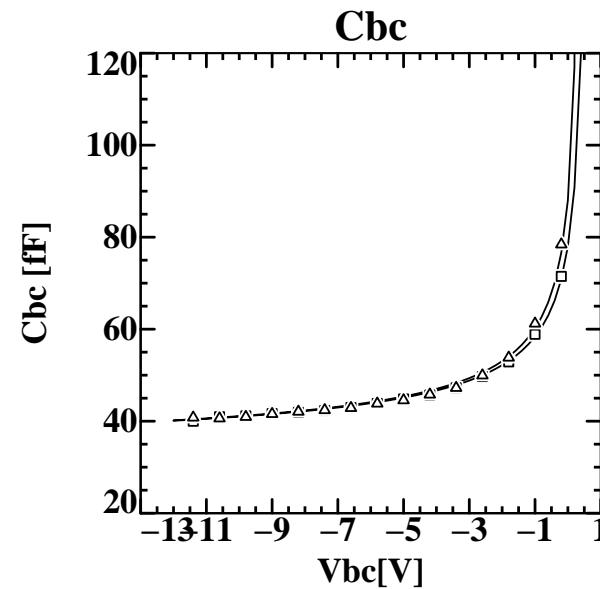
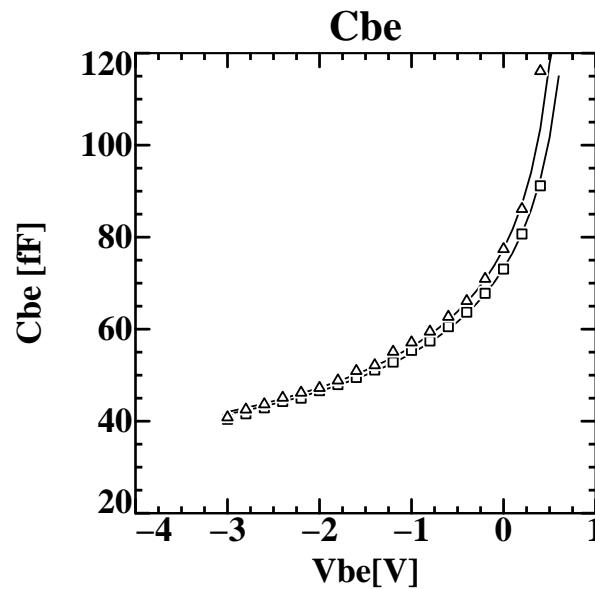


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- Previous CMC: Mextram 503 gives generally good results.
- Why Mextram 504
 - Modelling of SiGe processes
 - Easier and hence better parameter extraction
 - Better monotony in (higher) derivatives.
- We have tested Mextram 504 on five CMC data sets
- New parameter extraction only for process A

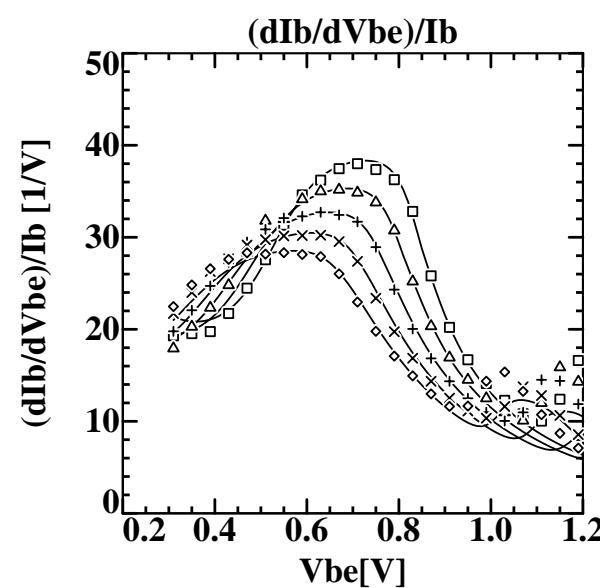
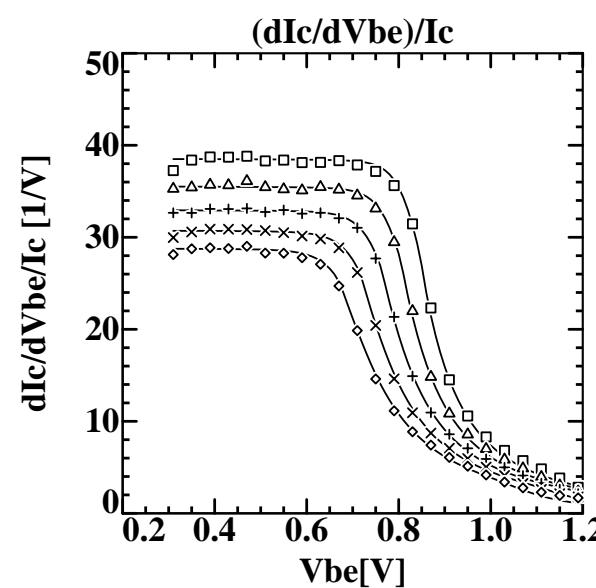
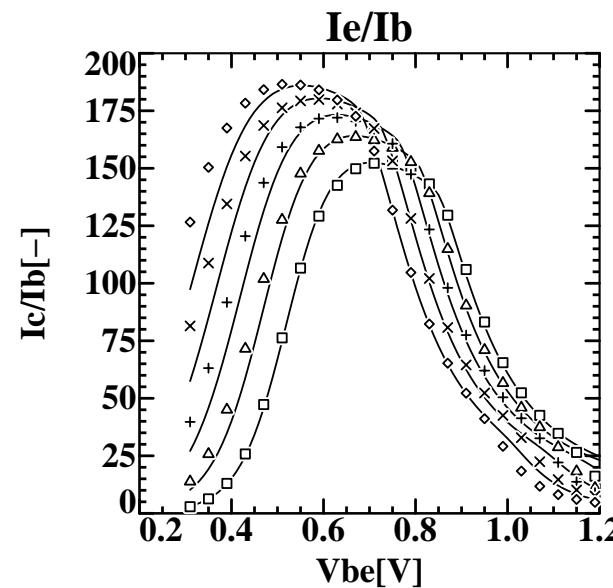
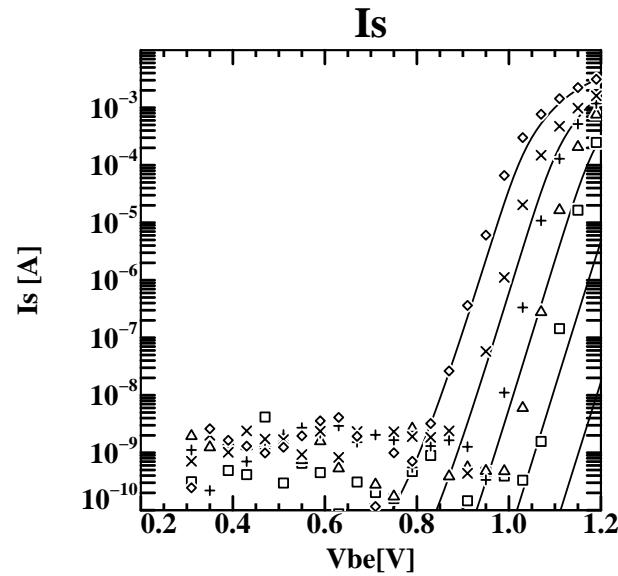
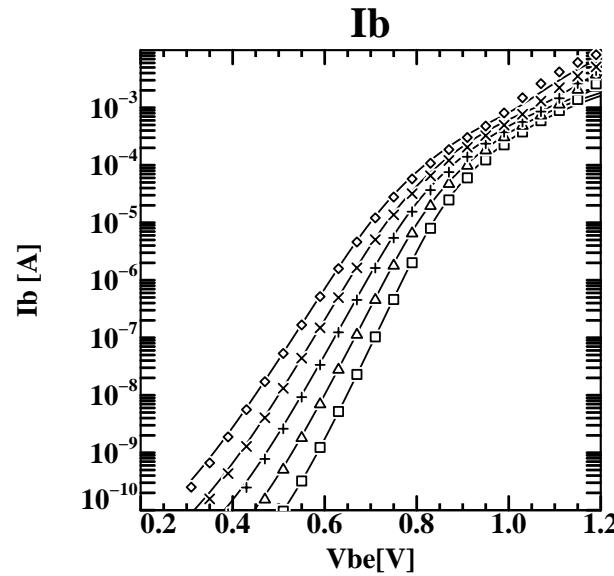
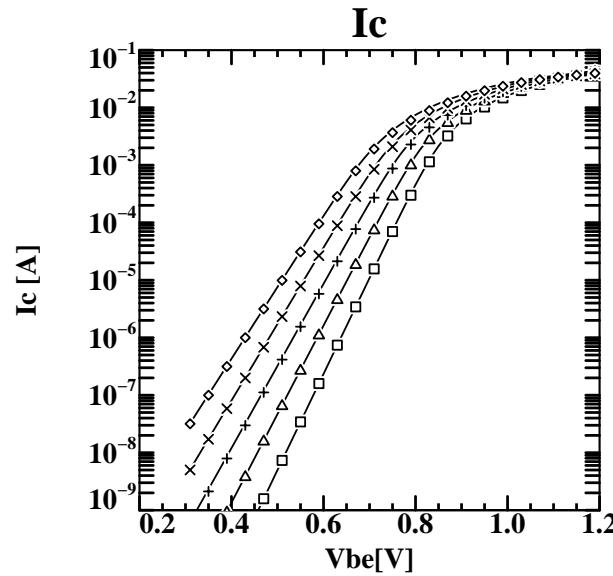
Process A: Cap Temp=25, 125 Mextram 503.2

(2)



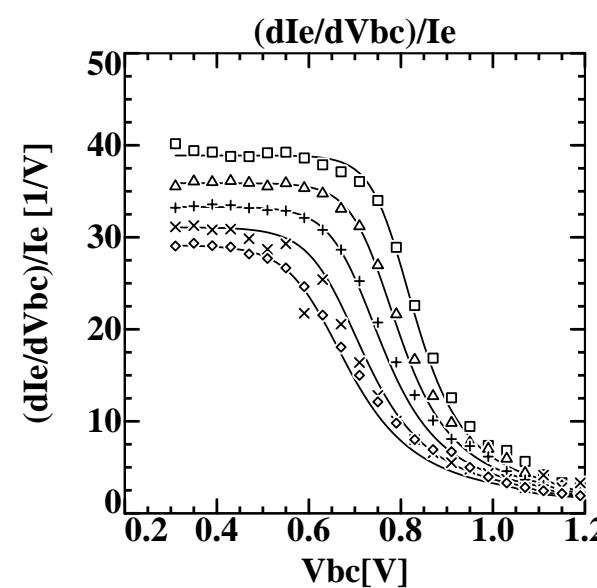
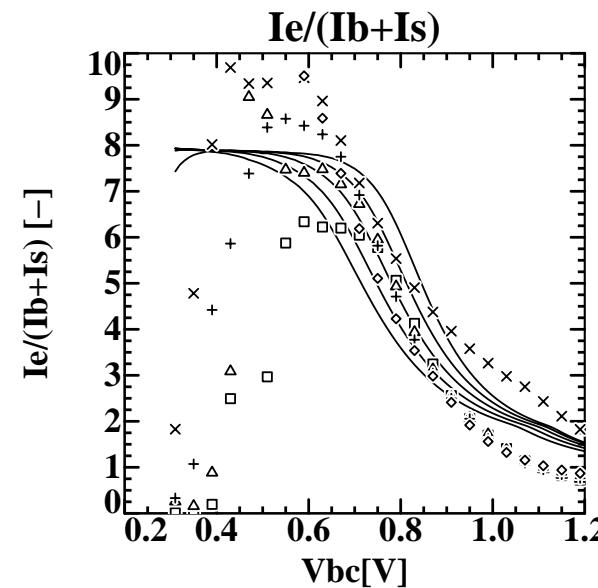
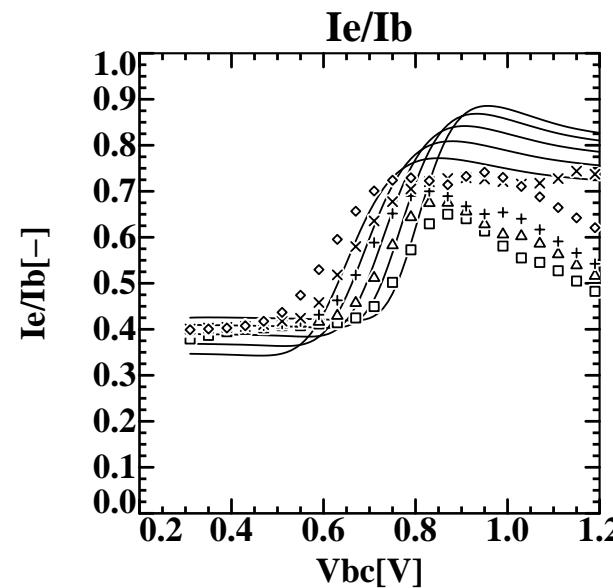
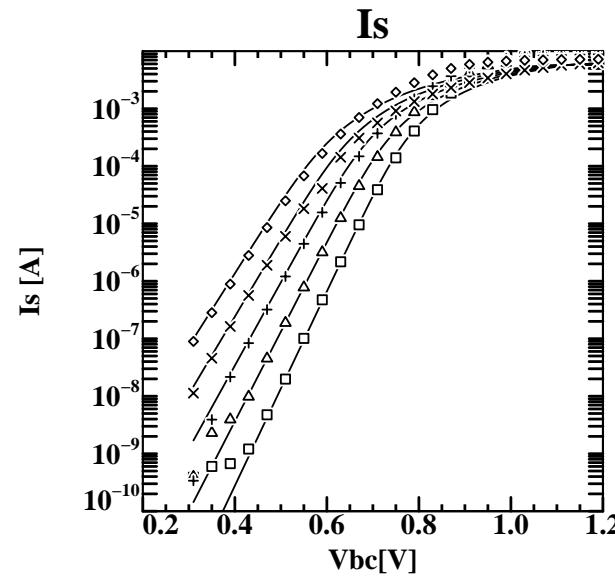
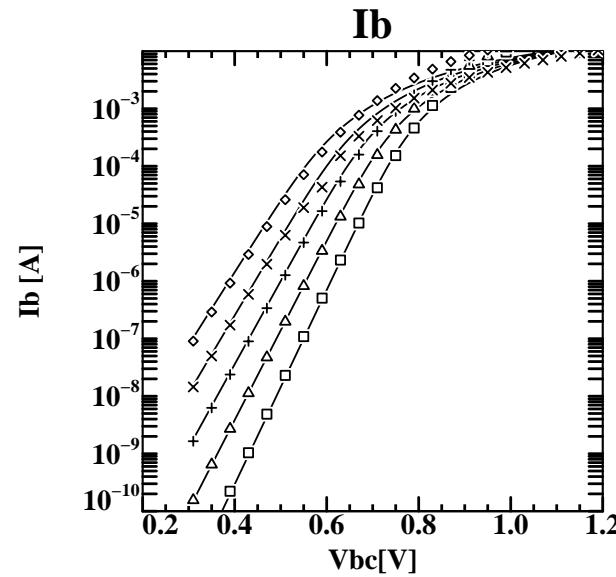
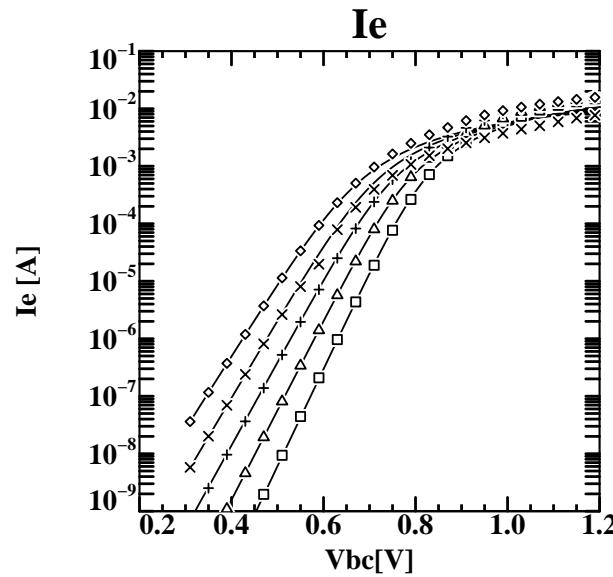
Process A: fgummel Vbc=0 Temp=25, 50, 75, 125, 150 Mextram 503.2

(3)

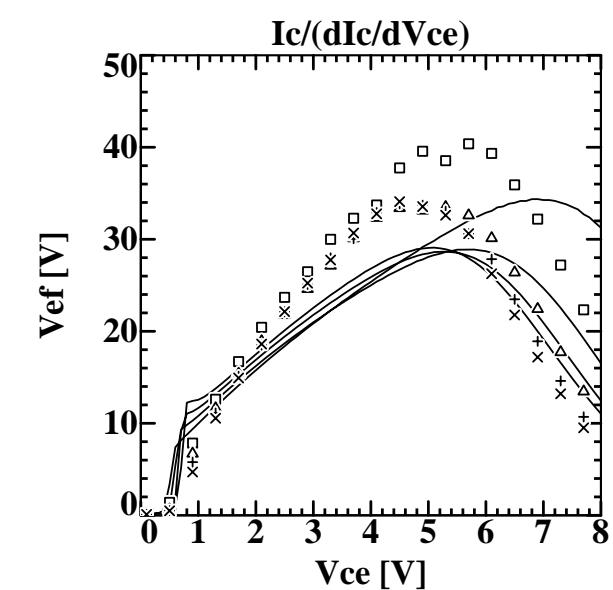
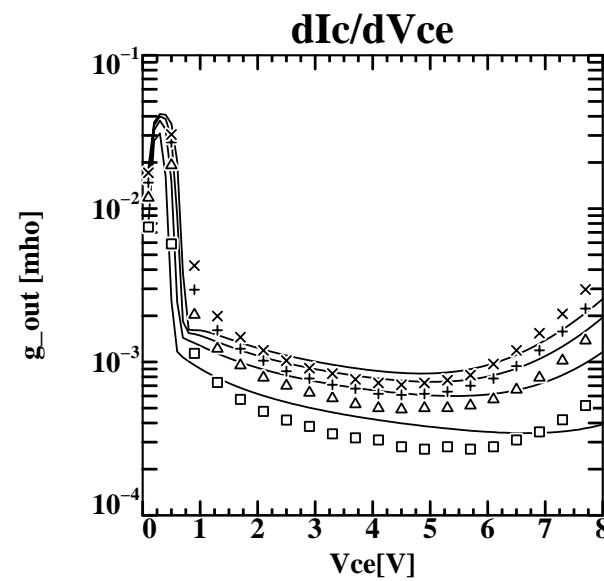
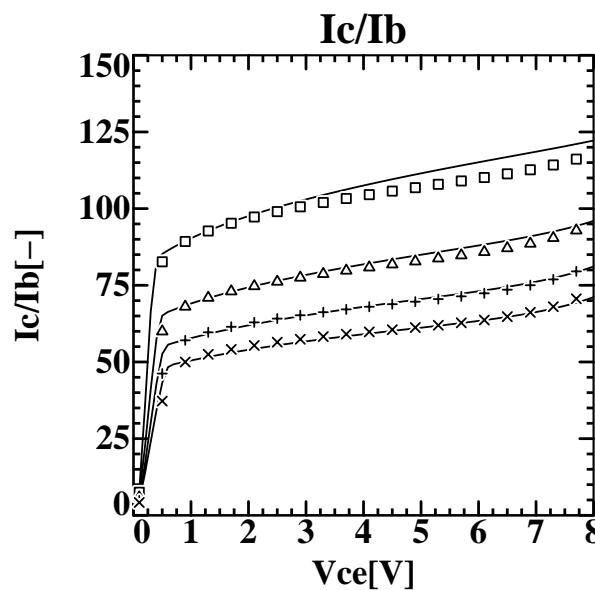
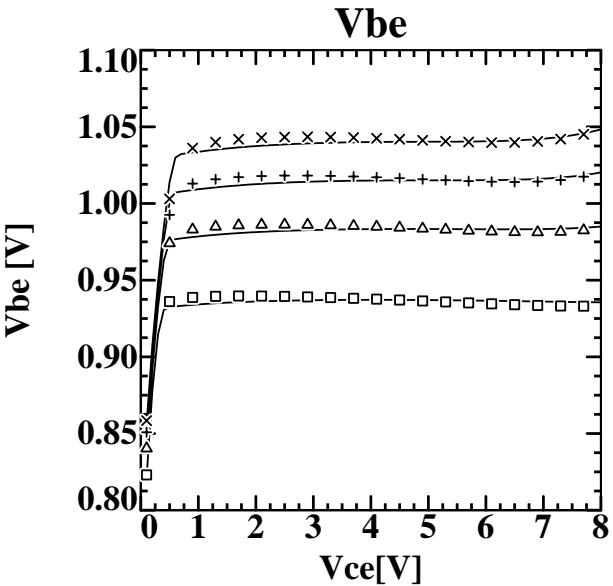
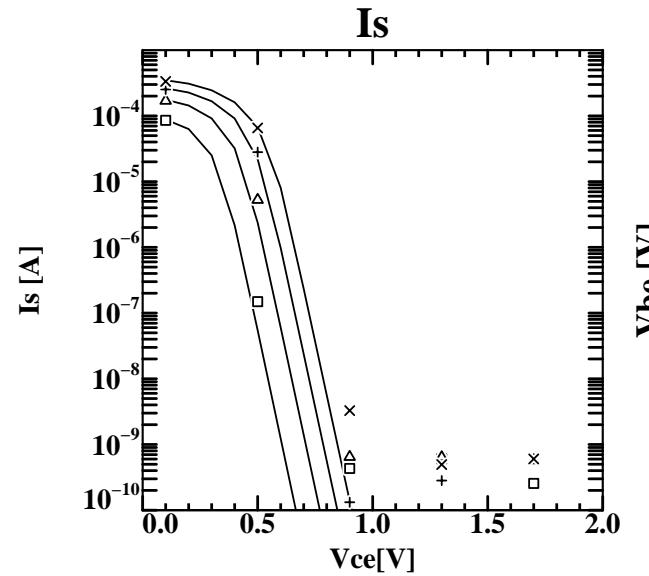
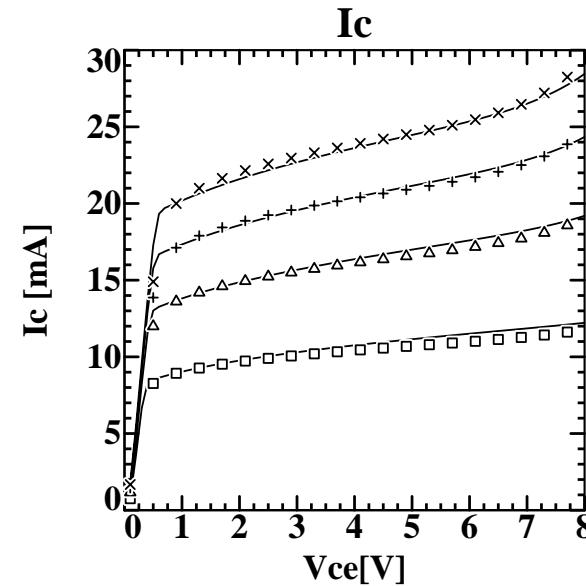


Process A: rgummel Vbe=0 Temp=25, 50, 75, 125, 150 Mextram 503.2

(4)

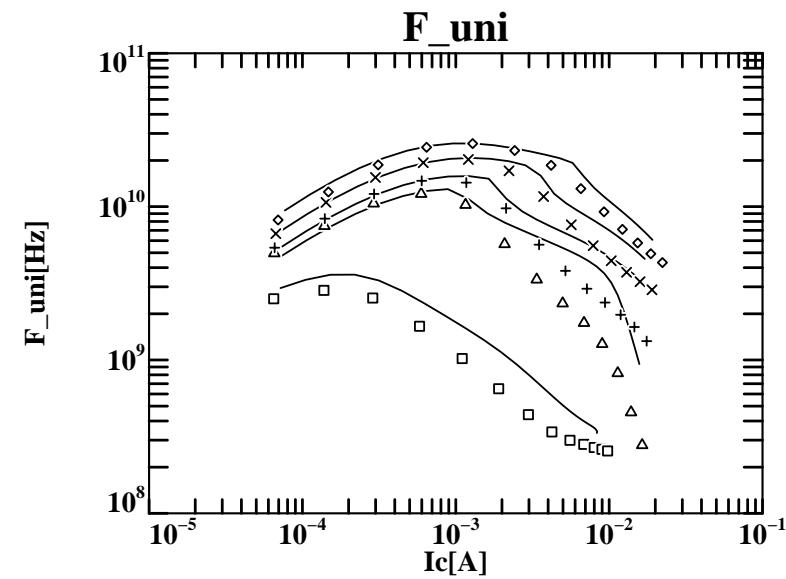
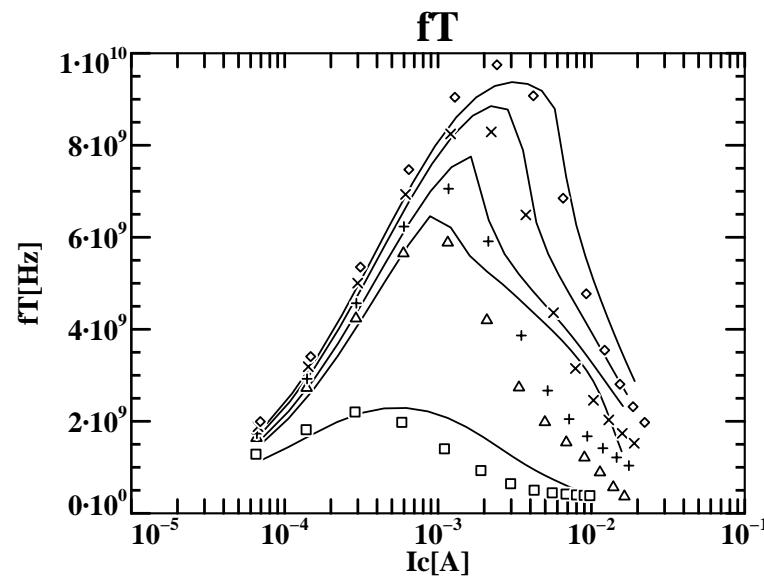
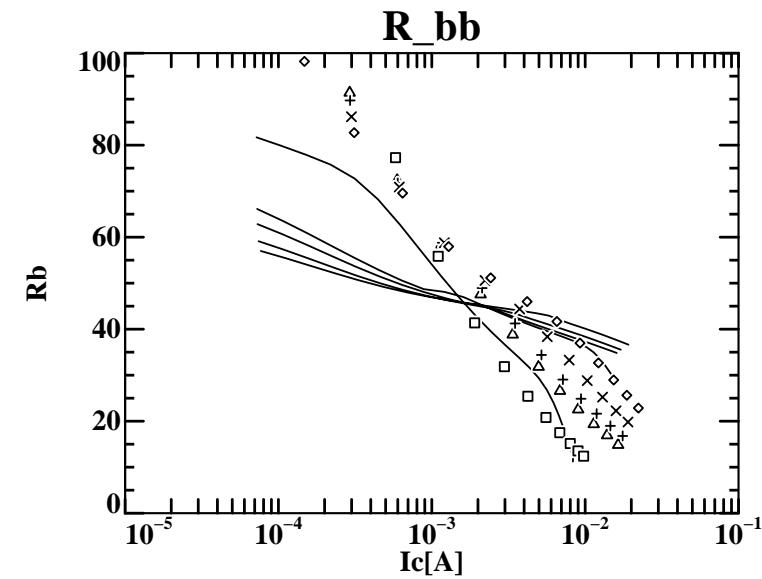
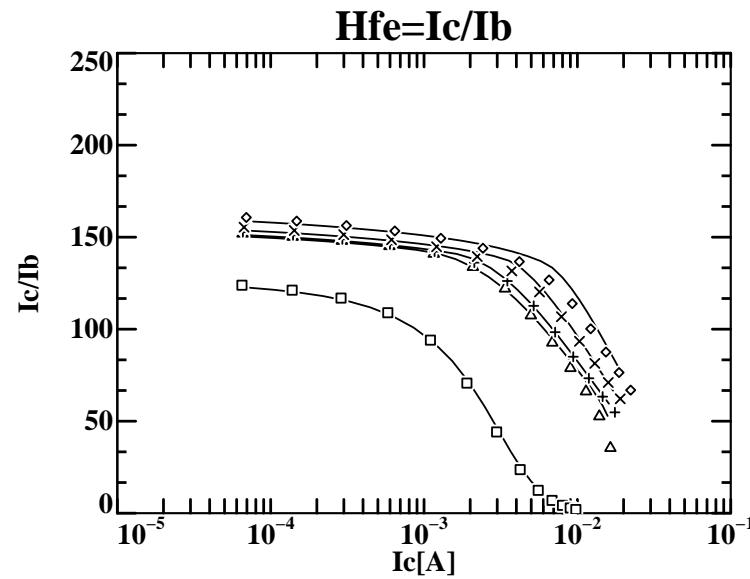


Process A: foutput-ib Temp=25 Ib=100, 200, 300, 400 uA Mextram 503.2 (5)



Process A: Temp=25 f=1 GHz, Vce =0.2, 0.5, 0.8, 2, 5 V Mextram 503.2

(6)



- Introduction and previous Mextram 503 results
- Reformulation of the epilayer model
- Results
- Conclusions

Process A

$V_{CE} = 0.2, 0.5, 0.8, 2.0, 5.0$

Single Poly BiCMOS process

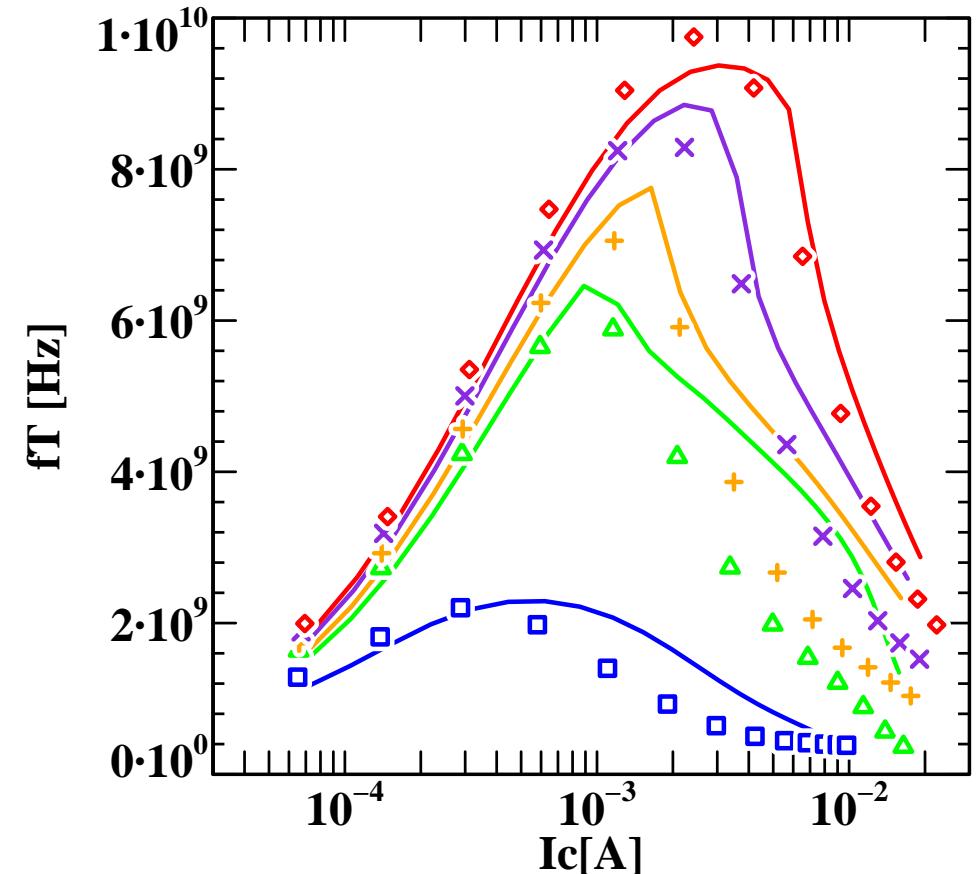
Emitter size: $0.6 \times 5.4 \mu\text{m}$

Double base contact: $r_p = 10 \text{ k}\Omega$

Maximum cut off frequency f_T

f_T : 10 GHz @ $V_{CE} = 5 \text{ V}$

f_T : 6 GHz @ $V_{CE} = 0.5 \text{ V}$



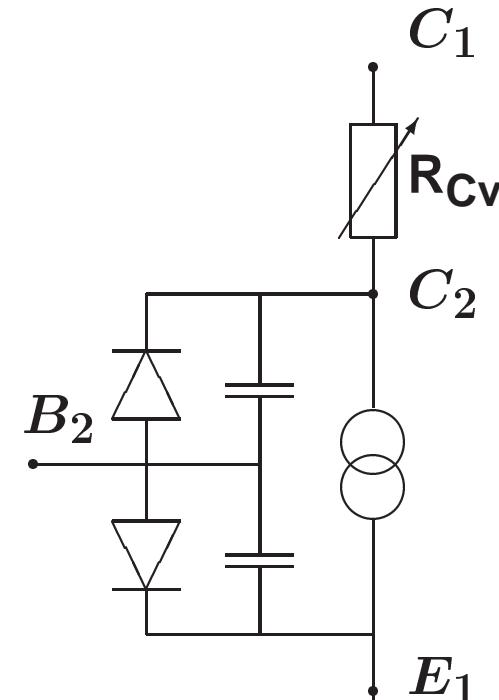
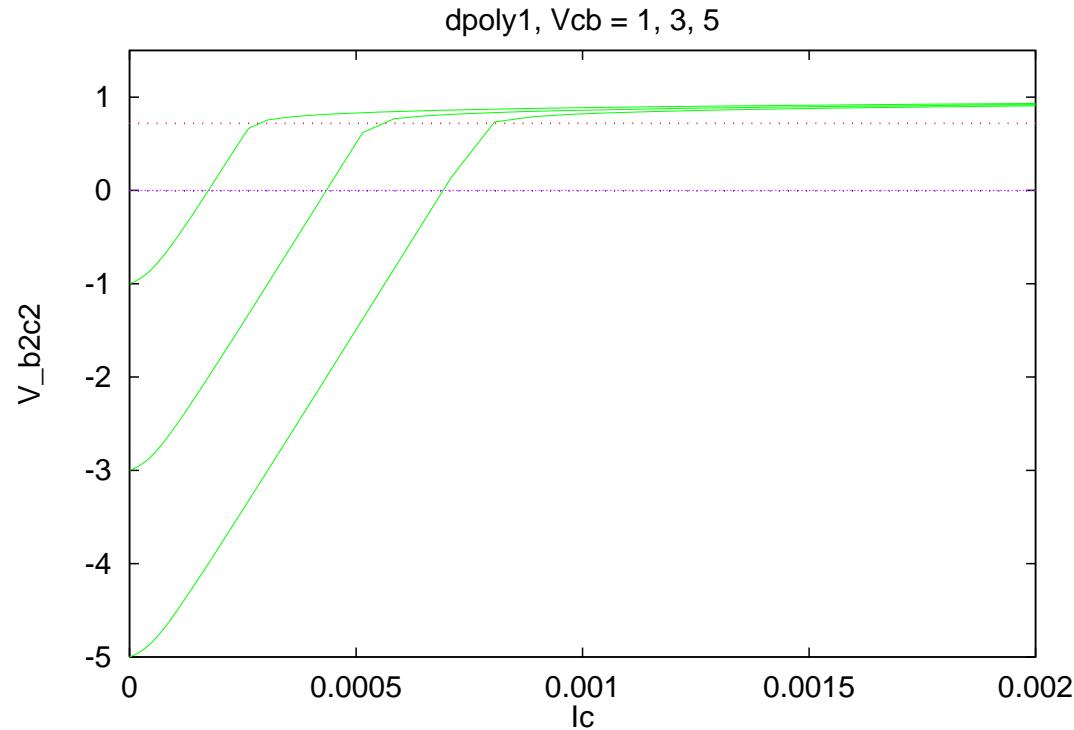
Internal base-collector bias

(9)

The internal base-collector bias increases **strongly** due to the (variable) epi-layer resistance.

When $V_{B_2C_2} > V_{d_C}$ the junction is open. The bias increases only **slightly**.

This happens quite abrupt.

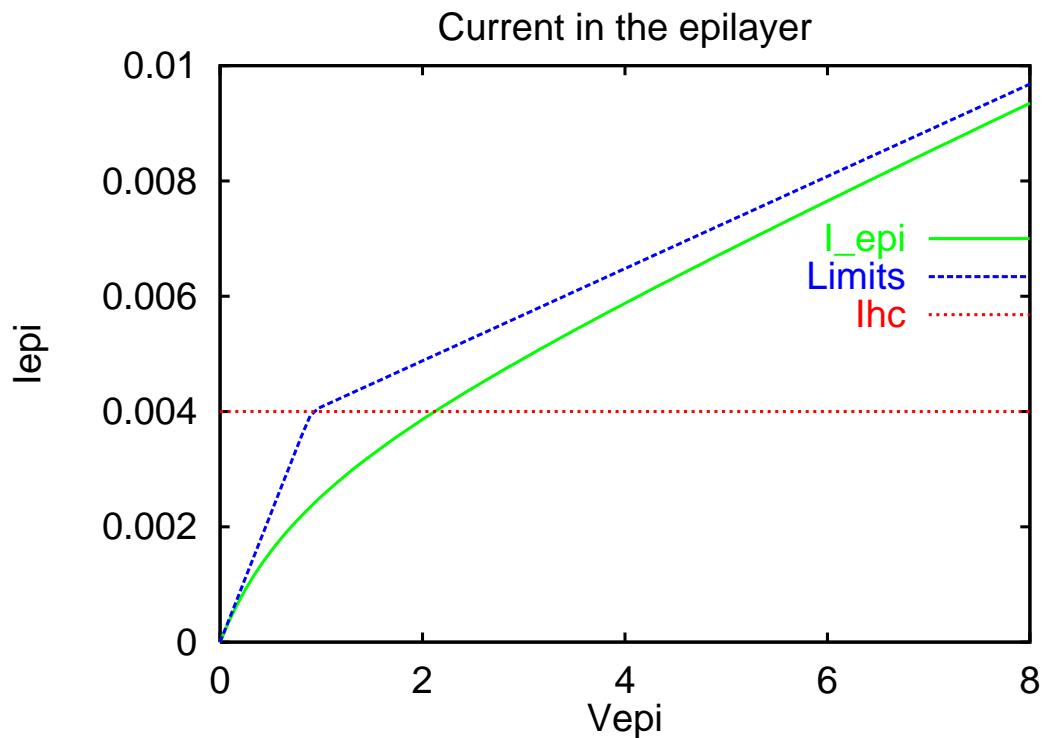


When there is no injection into the epilayer: ($\frac{x_i}{W_{\text{epi}}} = 0$)

$$V_{\text{epi}} = \mathcal{V}_{B_2C_2} - \mathcal{V}_{B_2C_1}$$

and

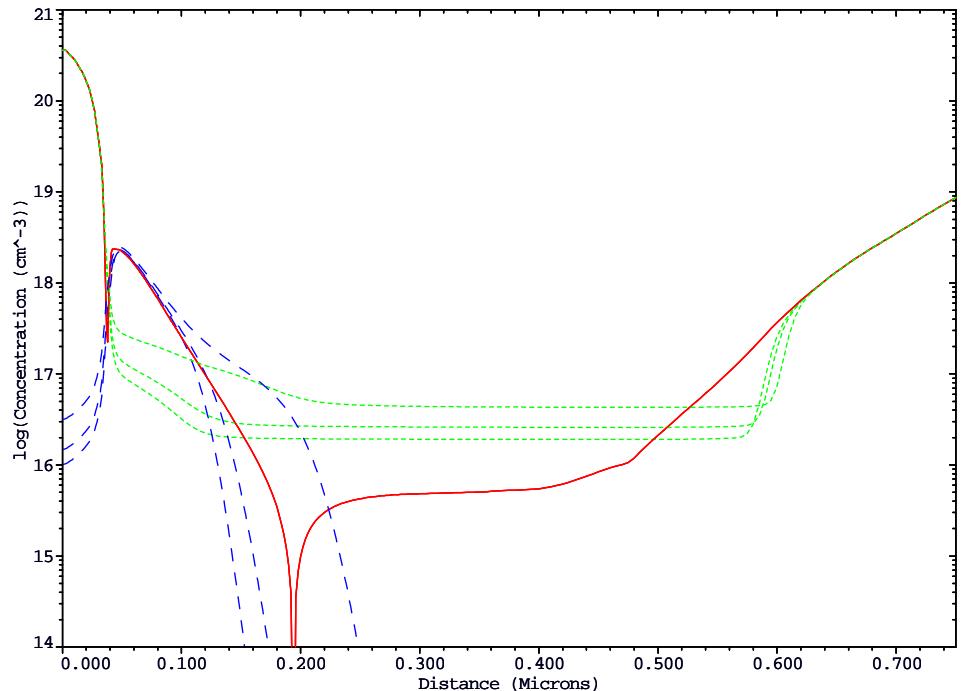
$$I = \frac{V_{\text{epi}}}{\text{SCR}_{\text{Cv}}} \frac{V_{\text{epi}} + I_{\text{hc}} \text{SCR}_{\text{Cv}}}{V_{\text{epi}} + I_{\text{hc}} R_{\text{Cv}}}$$



Basics of the epilayer model

(11)

$V_{ce} = 5V$; $V_{be} = 0.87, 0.88, 0.90V$; $I_c = 0.32, 0.44, 0.74 \text{ mA}$



In case of injection ($\frac{x_i}{W_{\text{epi}}} > 0$)

$$V_{\text{epi}} \simeq V_{dC} - V_{B_2C_1}$$

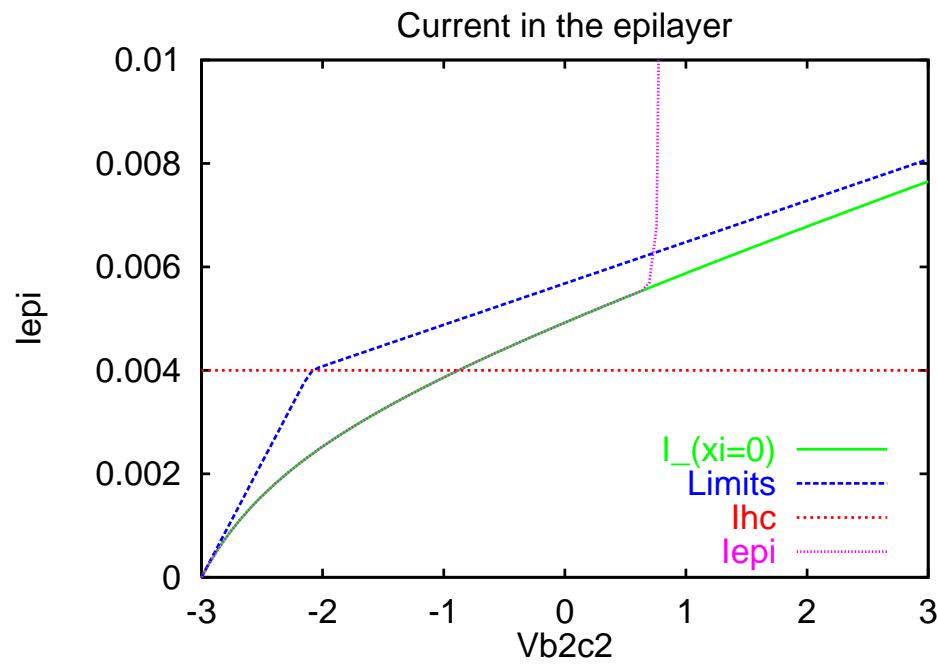
Injection thickness is given by
(Kull model)

$$\frac{x_i}{W_{\text{epi}}} = \frac{f(V_{B_2C_2}) - f(V_{B_2C_1})}{I_{C_1C_2} R_{Cv}}$$

$$I_{C_1C_2} = \frac{V_{\text{epi}}}{\text{SCR}_{Cv} \left(1 - \frac{x_i}{W_{\text{epi}}}\right)^2} \frac{V_{\text{epi}} + I_{hc} \text{SCR}_{Cv} \left(1 - \frac{x_i}{W_{\text{epi}}}\right)^2}{V_{\text{epi}} + I_{hc} R_{Cv} \left(1 - \frac{x_i}{W_{\text{epi}}}\right)}$$

Voltages $\mathcal{V}_{B_2C_2}$ and $\mathcal{V}_{B_2C_1}$ are given.

Combine the equations to find a third order equation for $I_{C_1C_2}$.



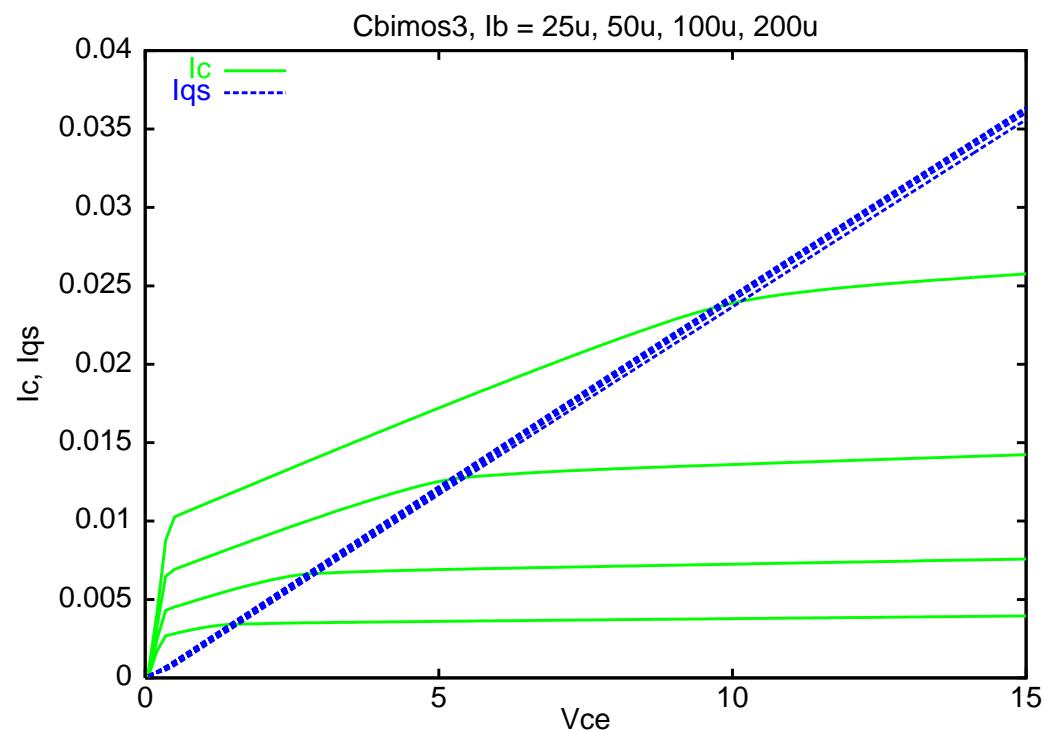
From $\mathcal{V}_{B_2C_2}$ calculate

- Reverse current I_r
 - Reverse base charge Q_{BC}
 - Epilayer charge Q_{epi}
(from charge control relation)
- Uses also $\mathcal{V}_{B_2C_1}$ and $I_{C_1C_2}$)

Injection starts when $V_{B_2C_2} \simeq V_{d_C}$:

$$V_{qs} \equiv V_{d_C} - V_{B_2C_1}$$

$$I_{qs} \equiv \frac{V_{qs}}{SCR_{Cv}} \frac{V_{qs} + I_{hc} SCR_{Cv}}{V_{qs} + I_{hc} R_{Cv}}$$

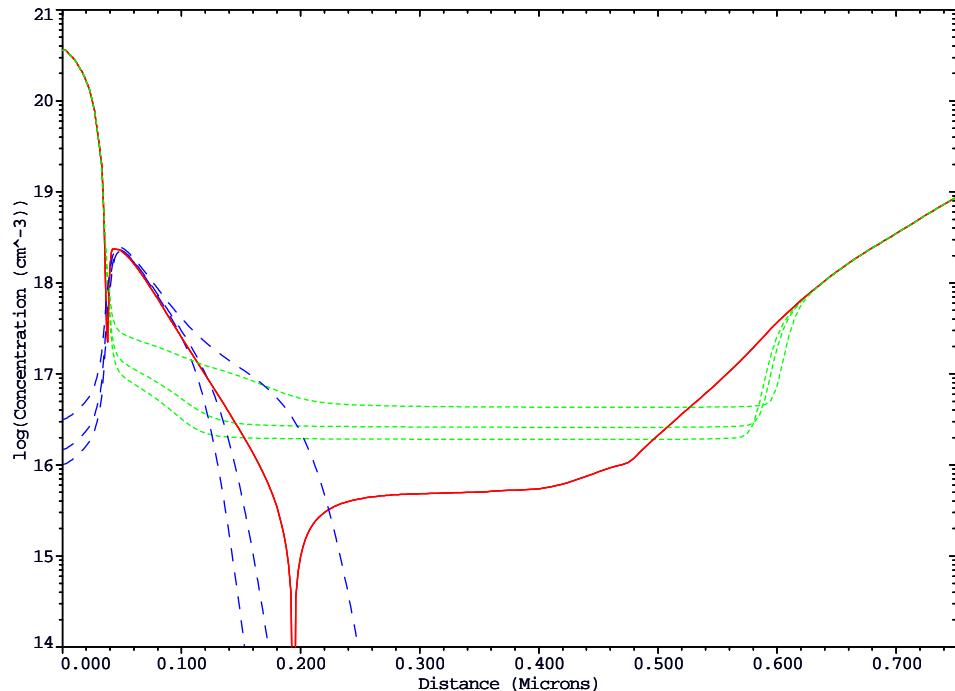


Example without velocity saturation

Basics of the epilayer model (recap)

(14)

$V_{ce} = 5V$; $V_{be} = 0.87, 0.88, 0.90V$; $I_c = 0.32, 0.44, 0.74 \text{ mA}$



In case of injection ($\frac{x_i}{W_{\text{epi}}} > 0$)

$$V_{\text{epi}} \simeq V_{dC} - V_{B_2C_1}$$

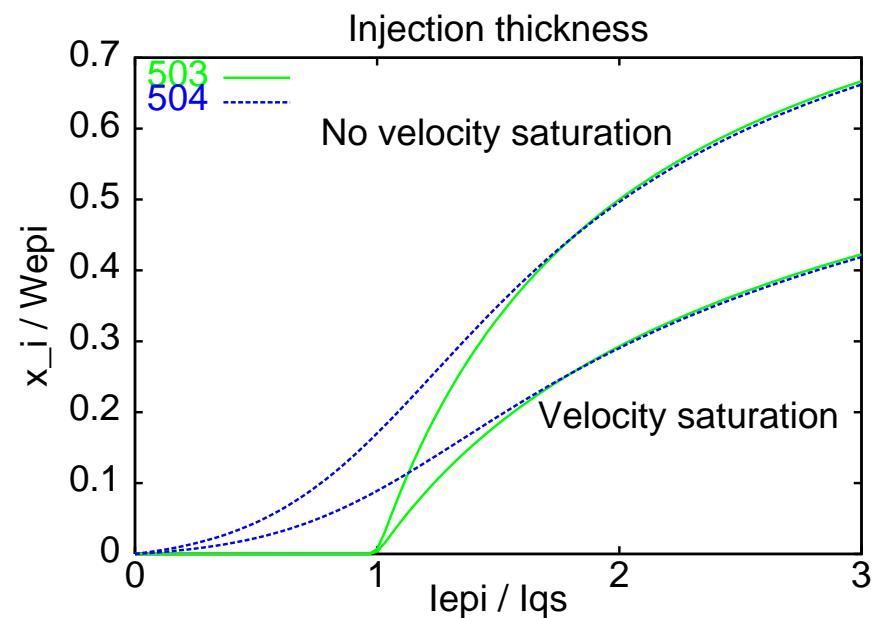
Injection thickness is given by
(Kull model)

$$\frac{x_i}{W_{\text{epi}}} = \frac{f(V_{B_2C_2}) - f(V_{B_2C_1})}{I_{C_1C_2} R_{Cv}}$$

$$I_{C_1C_2} = \frac{V_{\text{epi}}}{\text{SCR}_{Cv} (1 - \frac{x_i}{W_{\text{epi}}})^2} \frac{V_{\text{epi}} + I_{hc} \text{SCR}_{Cv} (1 - \frac{x_i}{W_{\text{epi}}})^2}{V_{\text{epi}} + I_{hc} R_{Cv} (1 - \frac{x_i}{W_{\text{epi}}})}$$

calculate $\frac{x_i}{W_{\text{epi}}}$ from $I_{C_1 C_2}$ and $V_{B_2 C_1}$ (third order equation)

$$\frac{x_i}{W_{\text{epi}}} = \begin{cases} 1 - \frac{I_{qs}}{I_{C_1 C_2}} & \text{no velocity saturation} \\ 1 - \sqrt{\frac{I_{qs}}{I_{C_1 C_2}}} & \text{velocity saturation} \end{cases}$$



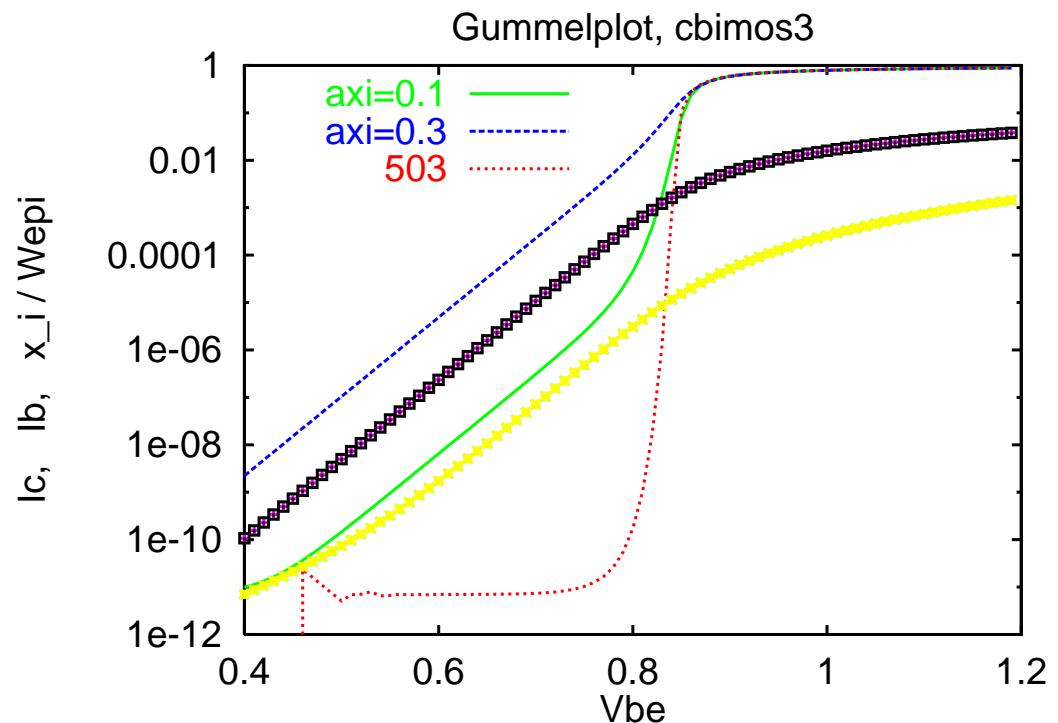
Calculate $\mathcal{V}_{B_2C_2}^*$ from the equation for $\frac{x_i}{W_{\text{epi}}}$ (Kull model approximated):

$$\frac{x_i}{W_{\text{epi}}} = \frac{f(\mathcal{V}_{B_2C_2}^*) - f(\mathcal{V}_{B_2C_1})}{I_{C_1C_2} R_{\text{cv}}}$$

From $\mathcal{V}_{B_2C_2}^*$ calculate

- Reverse current I_r
- Reverse base charge Q_{BC}
- Epilayer charge Q_{epi}

This describes also charge in
hard saturation ($I_{C_1C_2} \simeq 0$)



Question: How do we find $I_{C_1C_2}$?

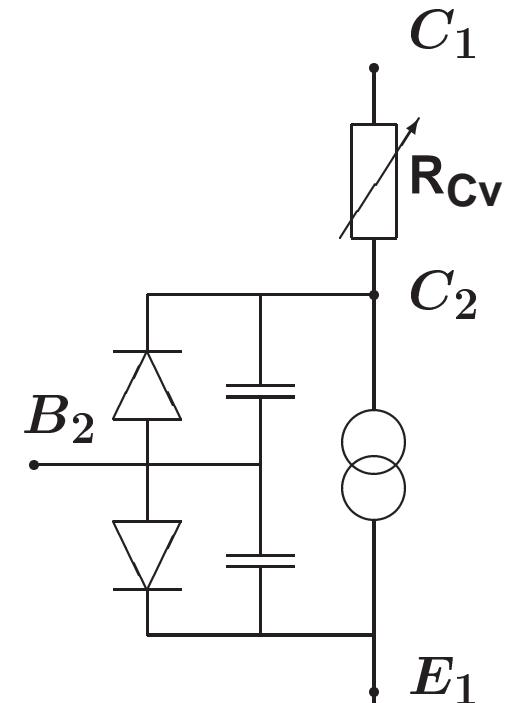
Use the epilayer resistance as a ***current sensor***.

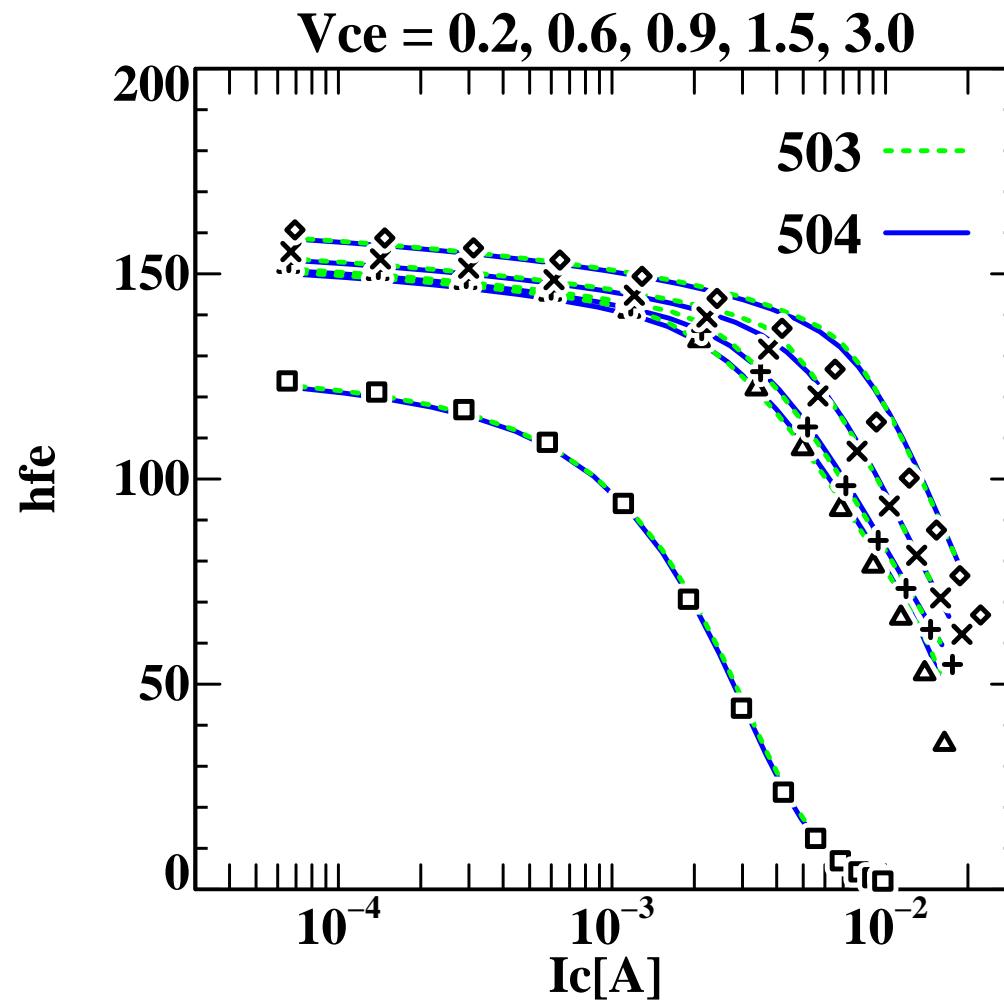
Node voltage $\mathcal{V}_{B_2C_2}$ is **only** used to define the current:

$$I_{C_1C_2} = \frac{f(\mathcal{V}_{B_2C_2}) - f(\mathcal{V}_{B_2C_1}) + \mathcal{V}_{C_1C_2}}{R_{Cv}}$$

(Kull model; also used in reverse)

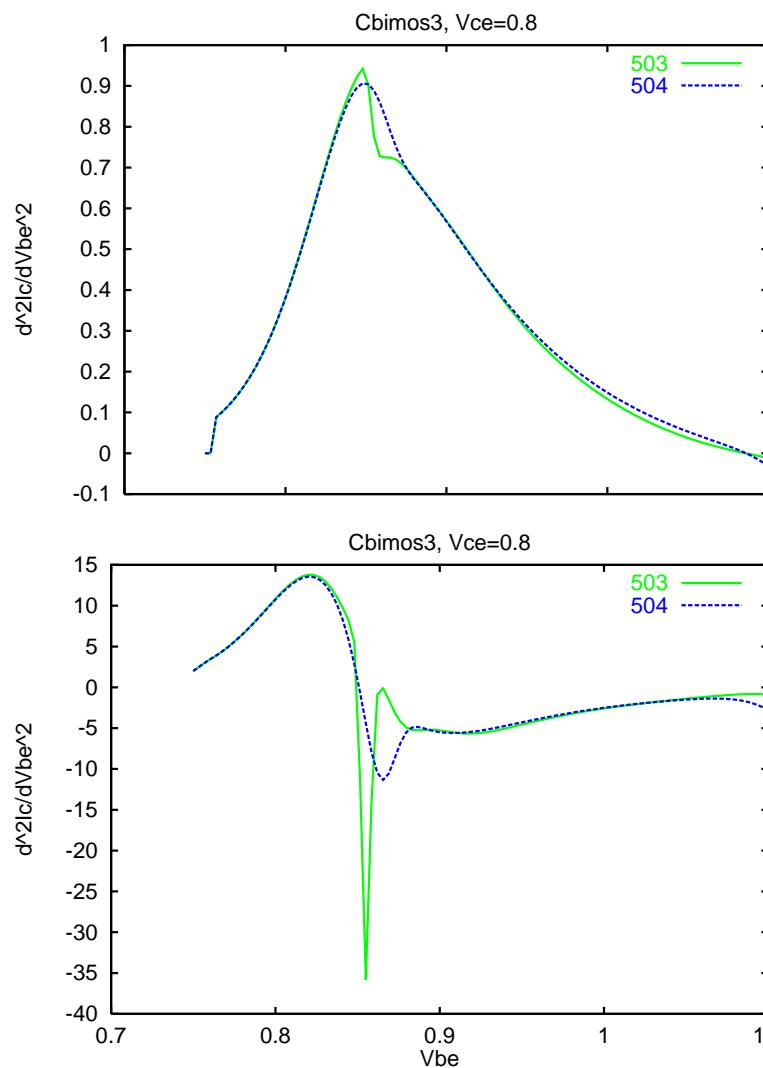
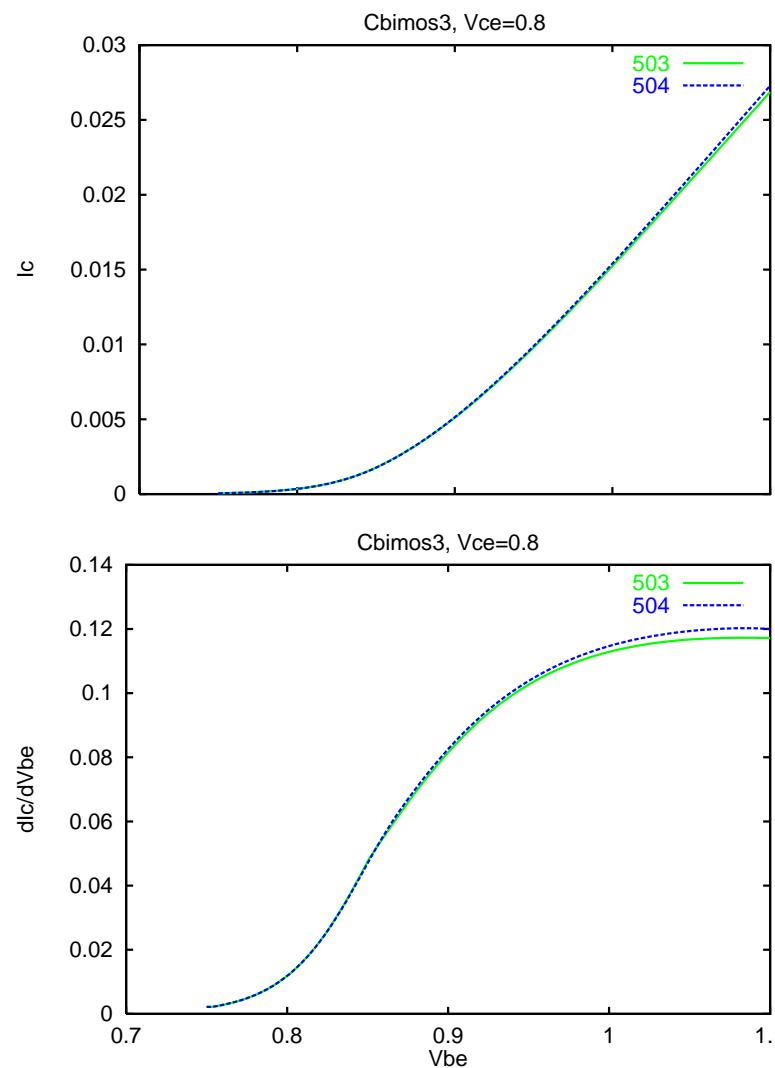
⇒ $\mathcal{V}_{B_2C_2}$ is always reasonably physical.

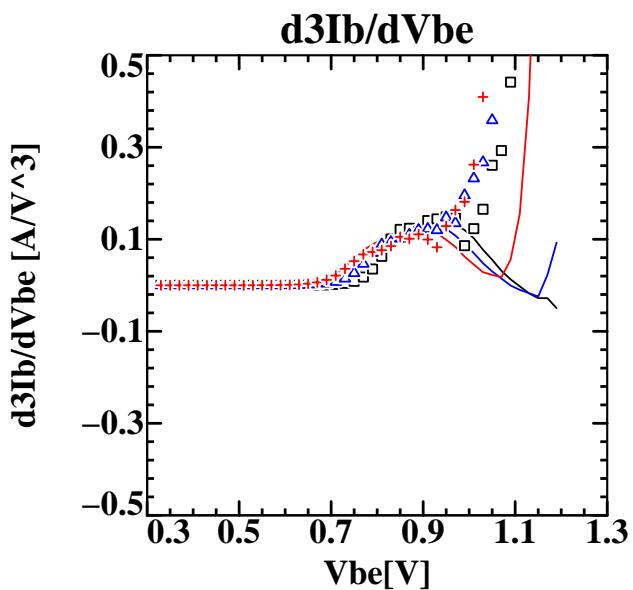
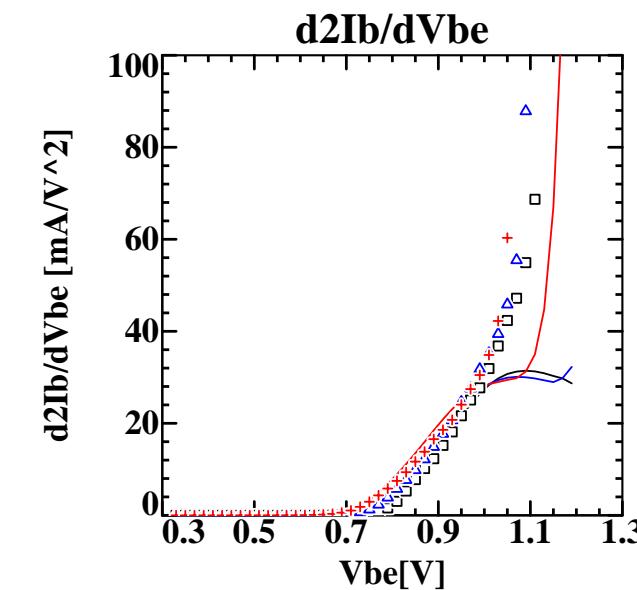
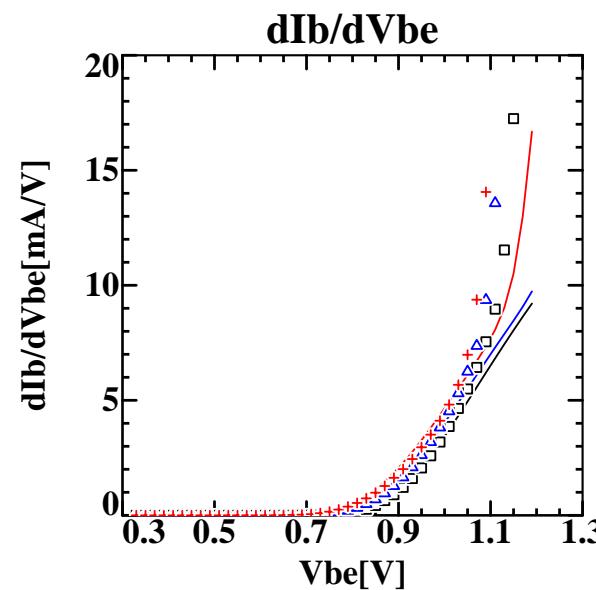
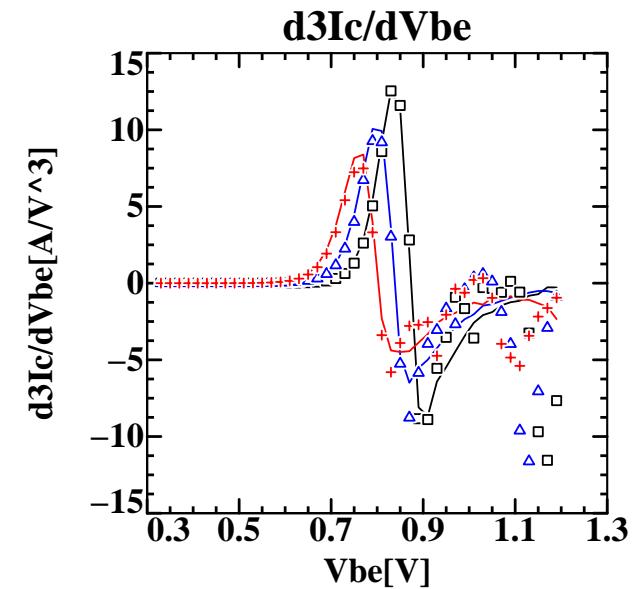
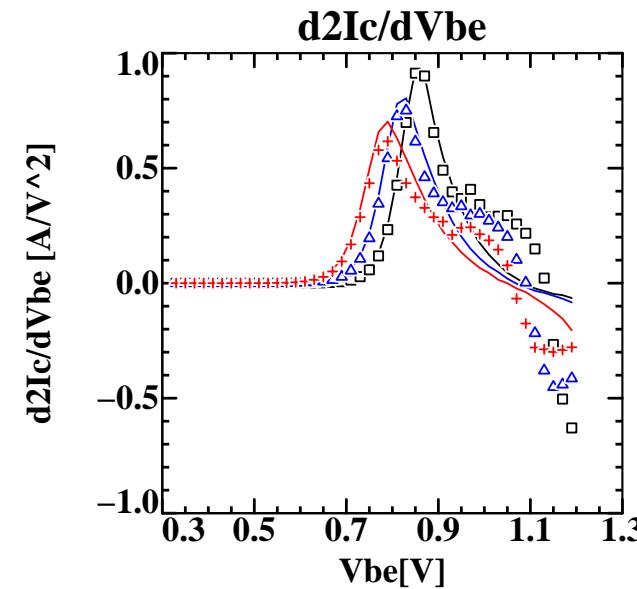
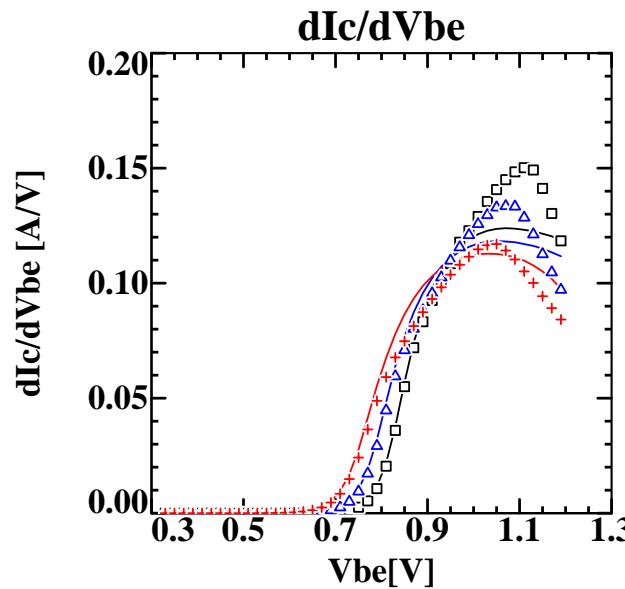


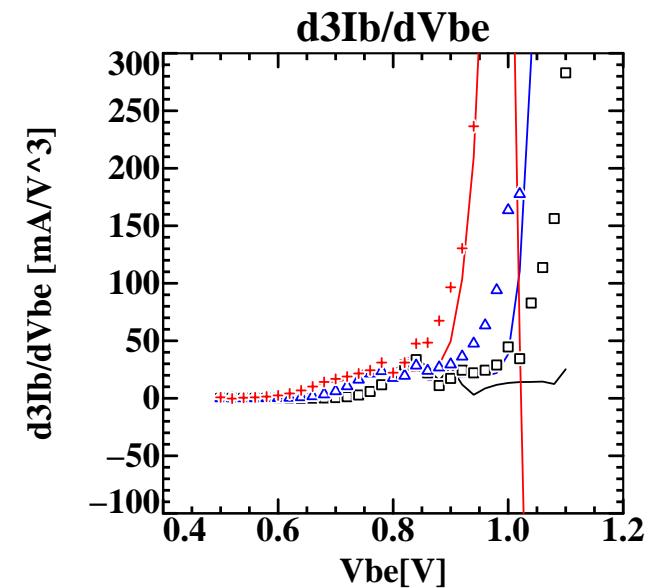
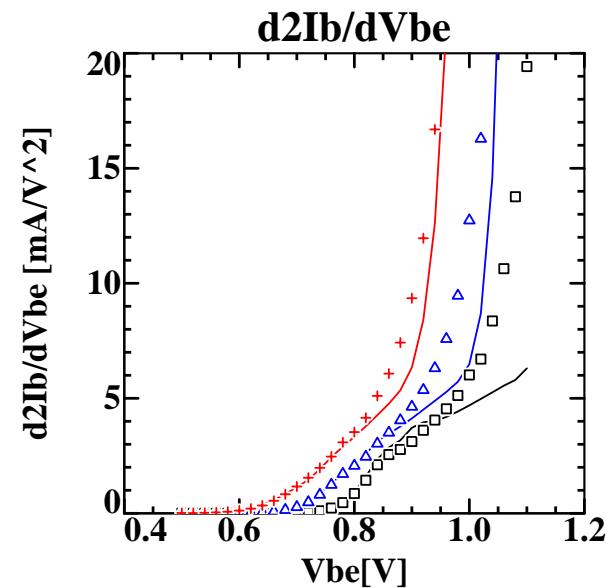
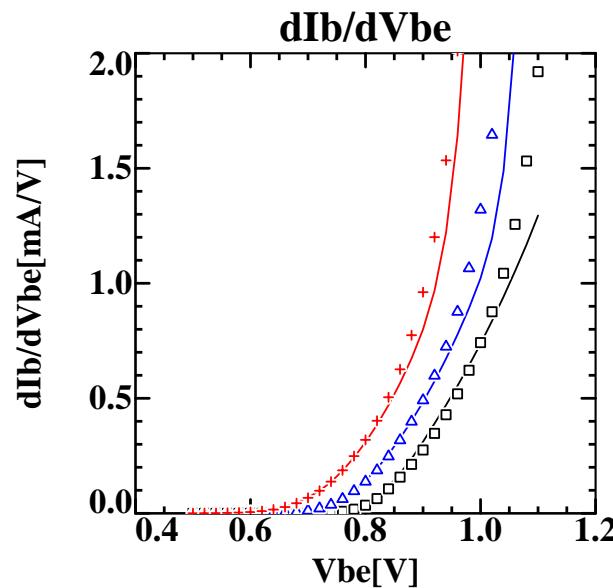
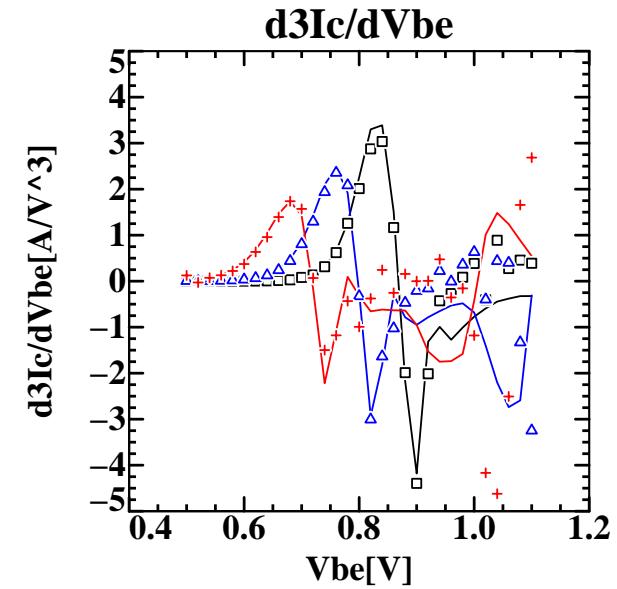
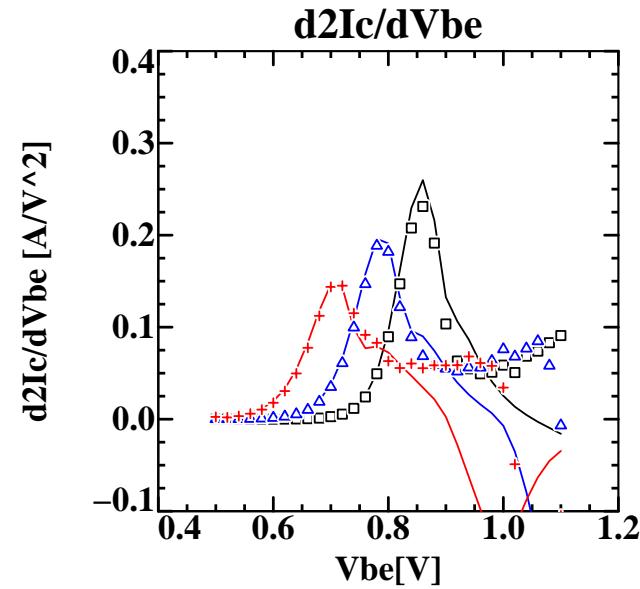
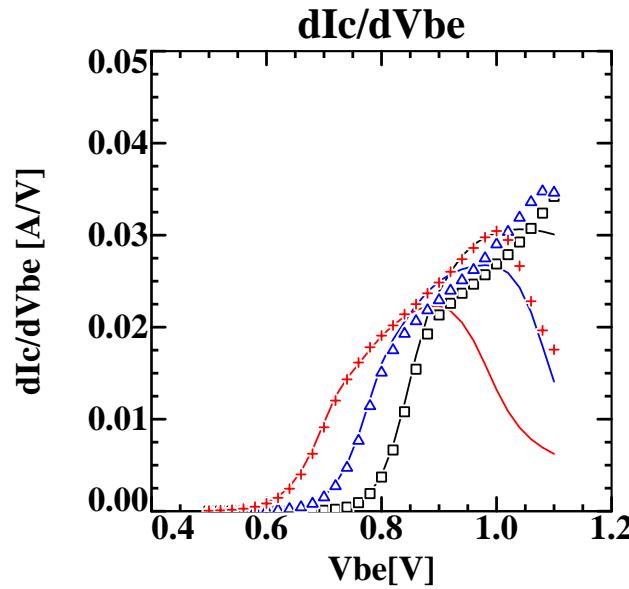


Current and derivatives

(19)

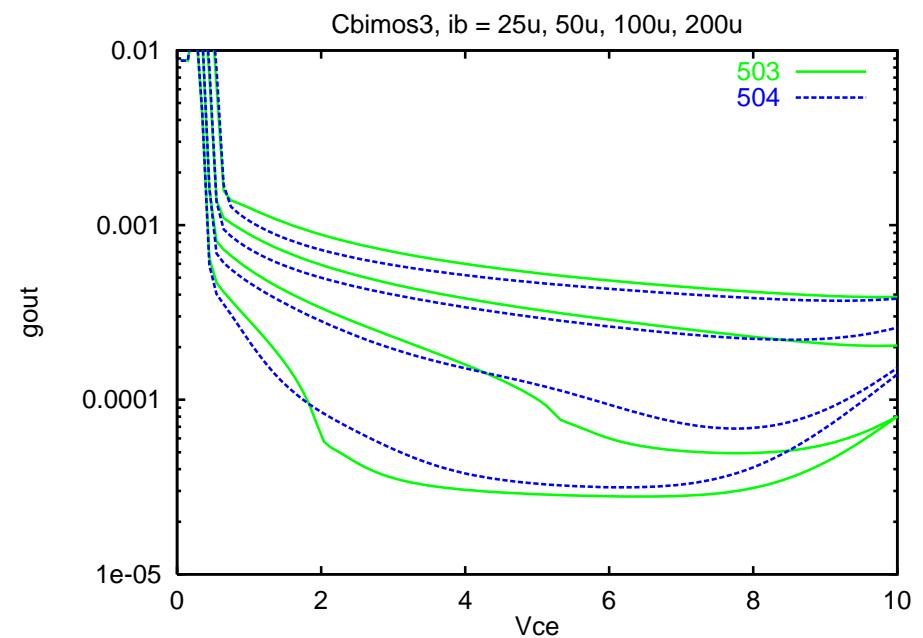
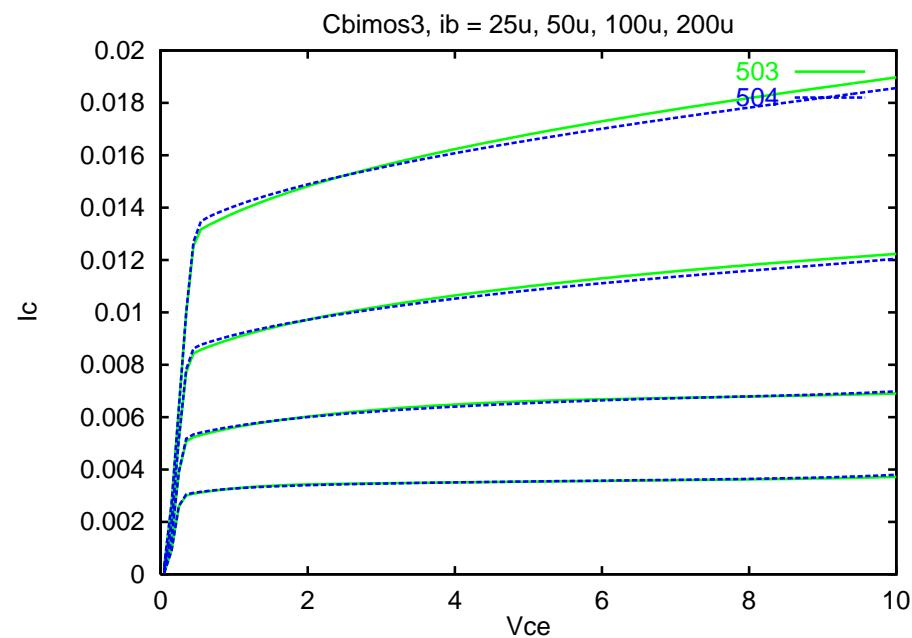




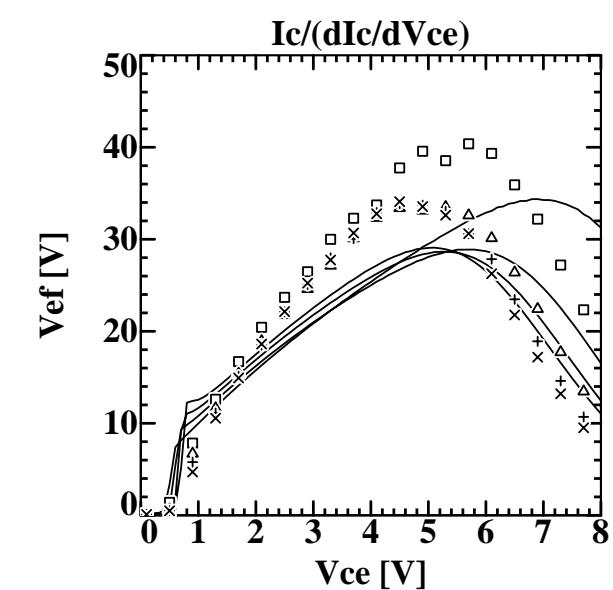
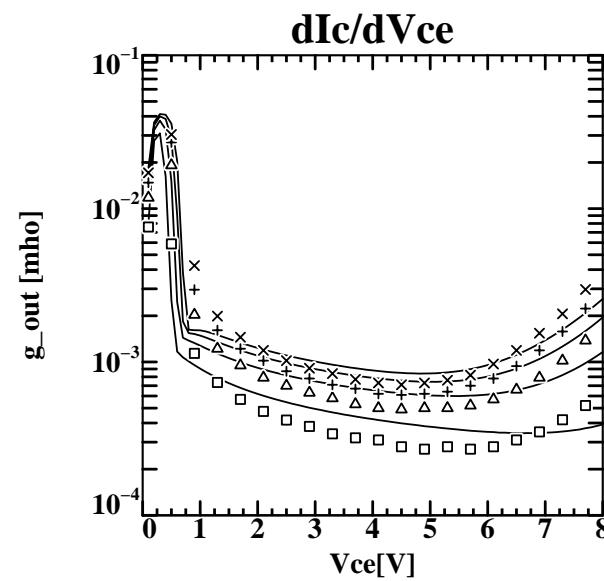
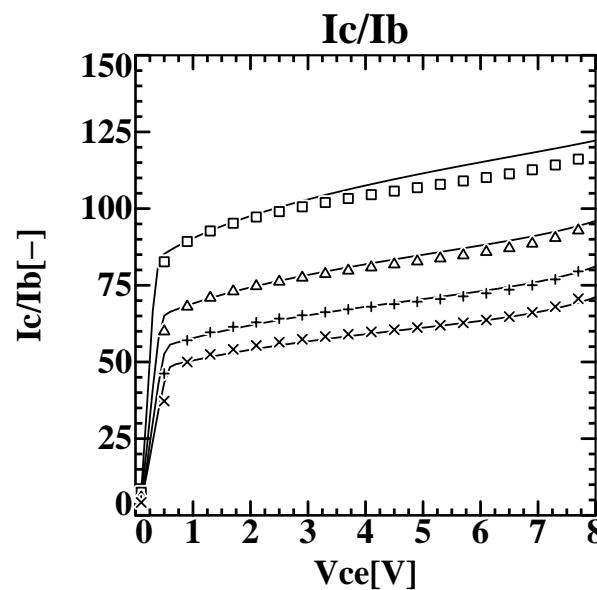
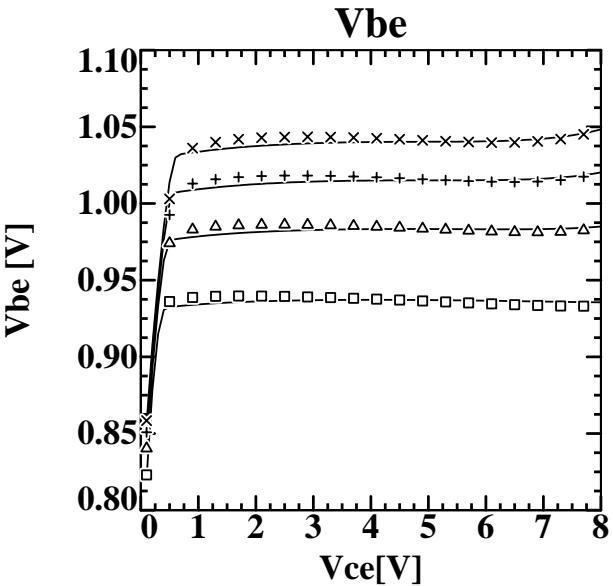
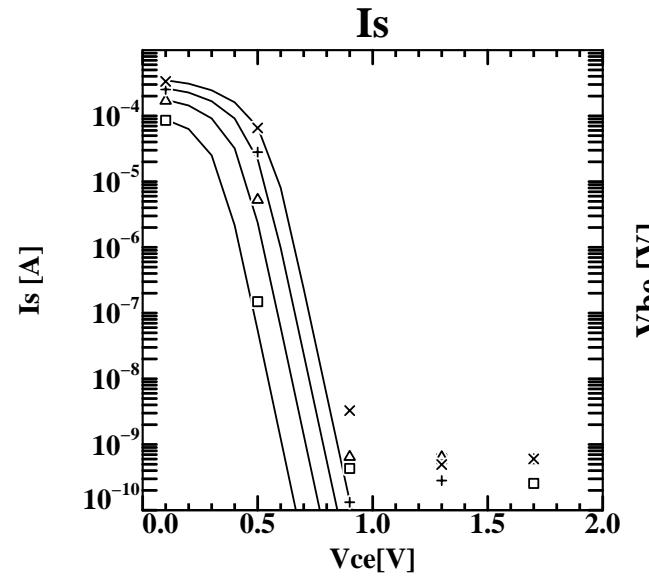
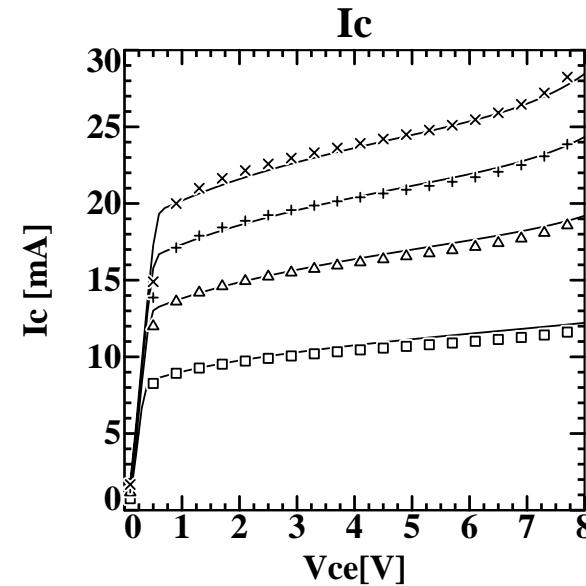


Output characteristics

(22)

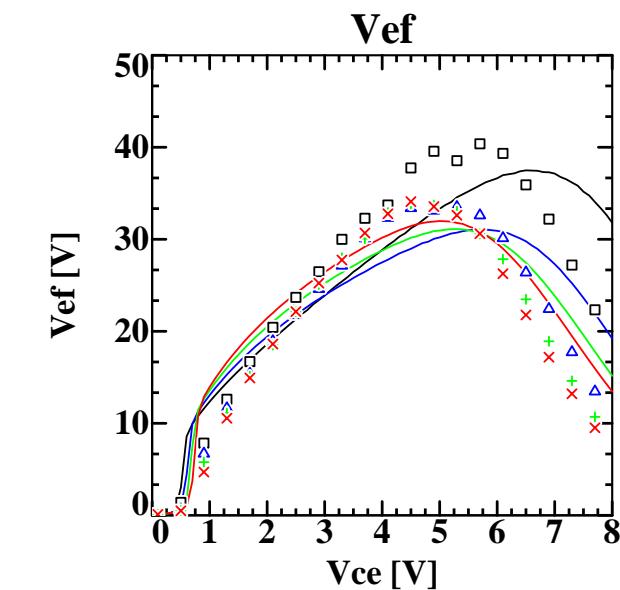
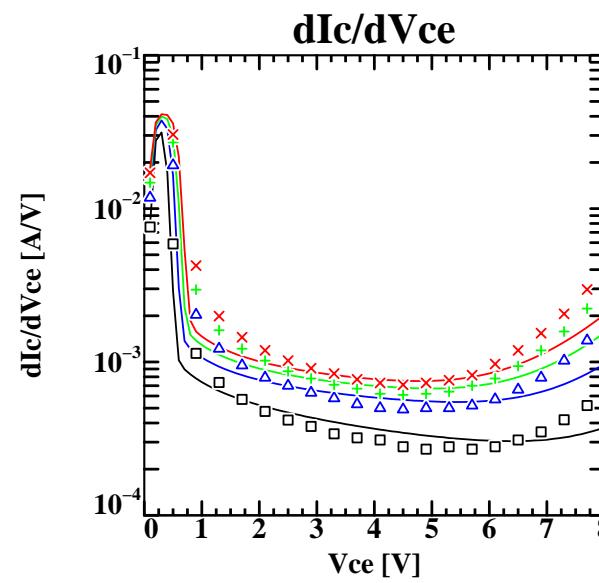
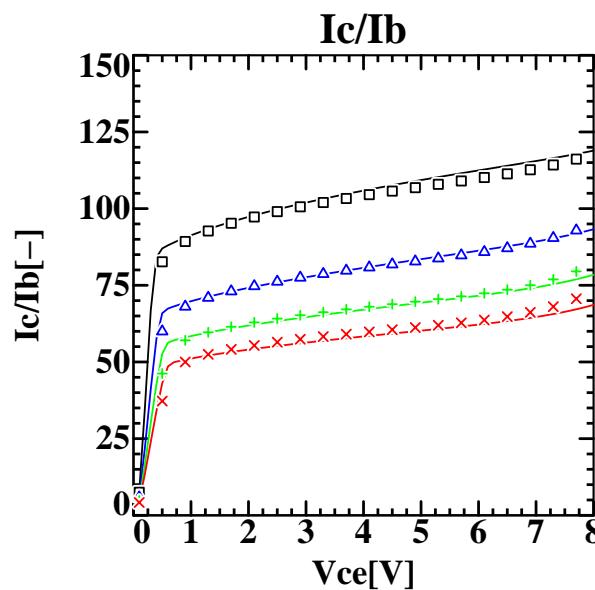
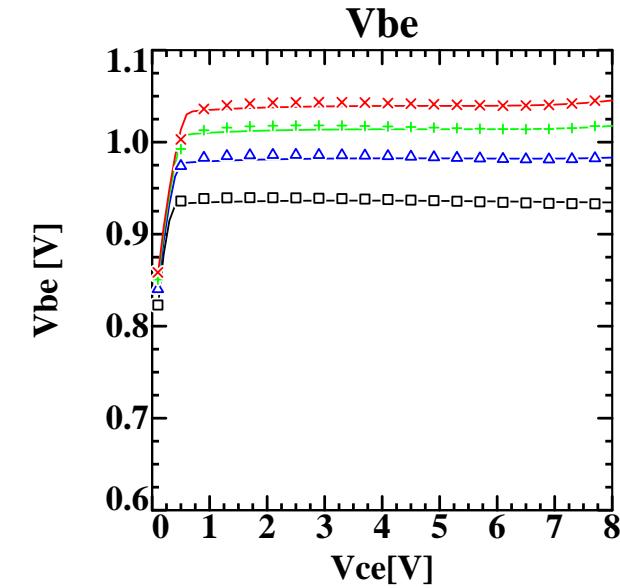
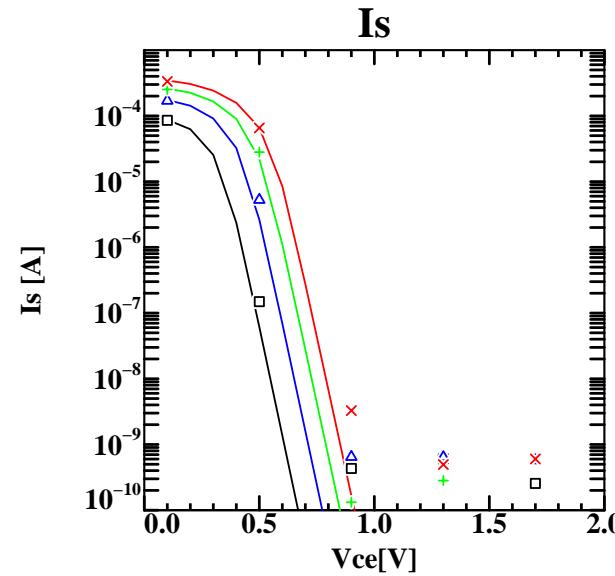
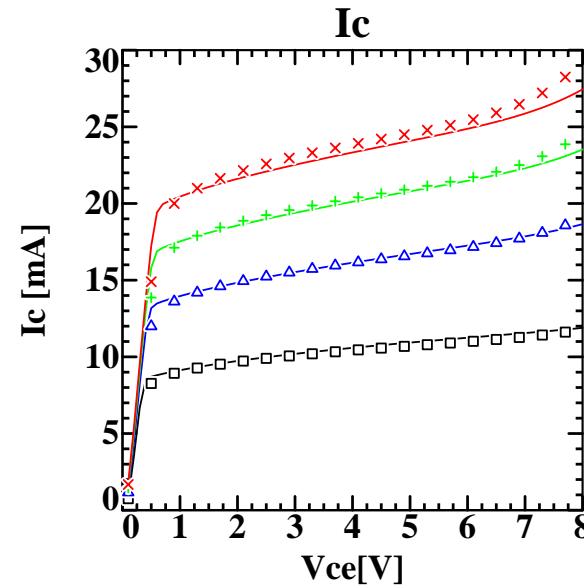


Process A: foutput-ib Temp=25 Ib=100, 200, 300, 400 uA Mextram 503.2 (23)

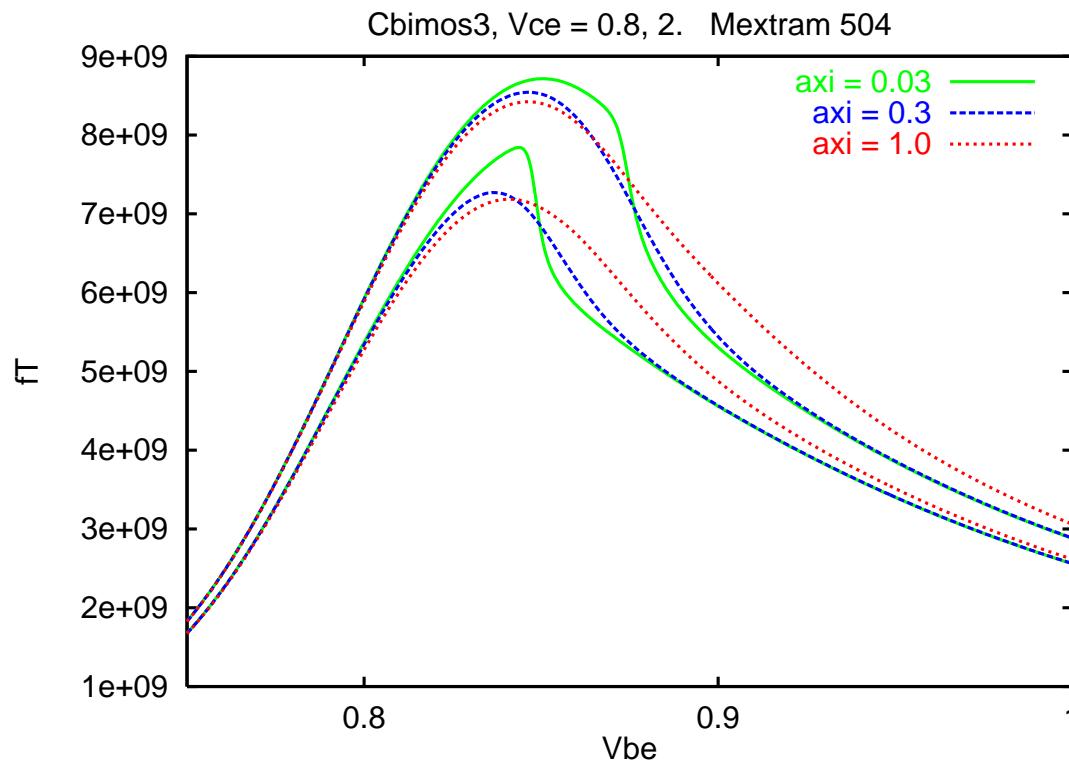


Process A: foutput-ib Temp=25 Ib=100, 200, 300, 400 uA Mextram 504

(24)

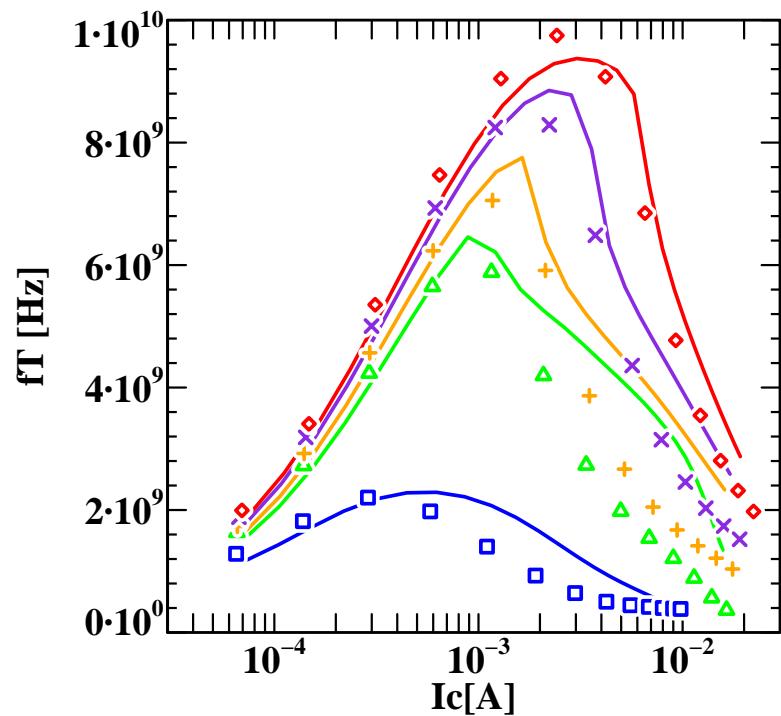


Basically we only need one new parameter: a_{x_i}

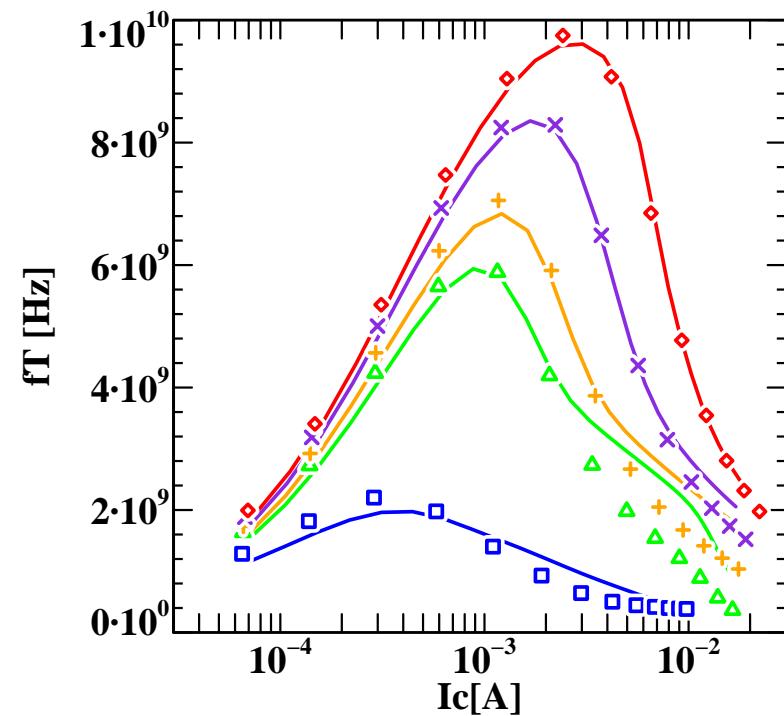


We also add the transit time parameters τ_B , τ_{epi} , and τ_R .
(In Mextram 503 these are calculated from DC parameters)

Mextram 503



Mextram 504



- Mextram 504 has much smoother characteristics
- Better description of measurements,
improved parameter extraction features must still be demonstrated.
- SiGe modelling:
 - Mextram 503 results are reasonable.
 - Physical description and geometric scaling better with Mextram 504
 - Not enough experience (yet) with SiGe (e.g. not tested in production)
- Mextram 504 will contain self-heating network
- Mextram 504 model equations are ready except for details
Further testing mainly within Philips